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Research paper



# Non-Linear Static Analysis of Off-Road Vehicle Cabin ROPS Structure Using Finite Element Method

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#### Abstract

The passive safety of operator is an important parameter to be evaluated when an automotive is considered. During life-threatening situations like vehicle rollovers, the safety of the operator can be ensured by the design of protective structure. The protective structure that safeguards the operator, is either an integral part of the cabin of the operator or an external structure outside the operator's compartment. The major accidents occurring in military, construction and mining operations are disastrous due to absence of this structure. Thus an effective ROPS (Roll Over Protective structure) along with the corresponding FOPS (Fall Over Protective Structure) can be used for saving lives.

Index Terms: Passive safety, Protective structure, ROPS, FEA.

### **1. Introduction**

In mining machines and heavy earthmovers there is a compartment, in which the operator operates. The protection of the compartment is vital, to save the lives of the operators and to avoid major fatal accidents. During operations, the life of operator comes into risk in a number of extreme situations. One of them is when moving over uneven earth surfaces the rolling of the machine takes place. Another one is, in mining caves, the heavy large pieces of earth masses falls over the compartment.

Thus the protective compartment must have the capacity to transfer the quantity of loads over it. The analysis result satisfies in accordance with the ISO standards.

### 2. Literature Review

During engineering work in construction and mining, protective structures are vital to provide safety to operator in case of a rollover (ROPS – ISO 3471) and to protect the construction machines against the falling objects (FOPS – ISO 3449). In the operations of mining machines, higher safety at impact energies must be ensured than the specified by ISO 3449. This is done because of the operating conditions and risks of rock slides. [1]

Depending on the applications, the operator's cabin must have adjustable height that increases the field view of the operator while drilling blast holes. But, a number of problems are caused in such structures to meet safety requirements defined in normative acts. Also, the mass of the machines extents up to 30,000 kg. Therefore, the ROPS should protect the residual space outlined by the DLV model. [2].

Myers and Pana-Cryan [3] related three strategies that prevents injuries experienced as an outcome of mining machine overturns. The three strategies were 'install FOPS, 'replace machines cabin' and 'do nothing'. They resolved that the preferred strategy in the case of cost effectiveness was the 'install FOPS' strategy on mining machines in which the FOPS were available. [4]

# **3.** Three Dimensional Cad Models and Meshing

The ROPS with ribs and without ribs are designed on the basis of required dimensions as per the safety norms. They are imported and meshed the images are shown below.



Fig. 1: ROPS without RIBS



Fig. 2: ROPS with RIBS



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Fig. 3: ROPS without RIBS Meshed



Fig. 4: ROPS with RIBS Meshed

### 4. Model Calculation

As per ISO 3471, the lateral load of 413918.89 N has been applied for the mass of 50000 Kg on the ROPS. The lateral load was found by the expression FL = 60000\*(M/10000)1.20.

# **5.** Comparision of ROPS with RIBS and Without Ribs

The structures are analyzed using ANSYS 15.0 to determine the total deformation for 6 different frequencies and 6 mode shapes are obtained.

The comparison results clearly suggest that deformation values of ROPS with RIBS are significantly lower compared to without RIBS. Below are the compared figures with caption.



Fig. 5: Total Deformation Mode 1 at 0HZ of ROPS without RIBS



Fig. 6: Total Deformation Mode 1 at 0HZ of ROPS with RIBS



Fig. 7: Total Deformation Mode 2 at 0HZ of ROPS without RIBS



Fig. 8: Total Deformation Mode 3 at 4.317e-003 HZ of ROPS without RIBS



Fig.9: Total Deformation Mode 4 at 7.8062e-003 HZ of ROPS without RIBS



Fig. 10: Total Deformation Mode 5 at 1.3685e-002 HZ of ROPS without RIBS



Fig.11: Total Deformation Mode 6 at 1.5841e-002 HZ of ROPS without RIBS



Fig. 12: Total Deformation Mode 2 at 0HZ of ROPS with RIBS



Fig.13: Total Deformation Mode 3 at 4.317e-003 HZ of ROPS with RIBS



Fig.14: Total Deformation Mode 4 at 7.8062e-003 HZ of ROPS with RIBS



Fig.15: Total Deformation Mode 5 at 1.368 5e-002 HZ of ROPS with RIBS



Fig.16 Total Deformation Mode 6 at 1.5841e-002 HZ of ROPS with RIBS

The table showing the values of frequencies at different modes for both ROPS without RIBS and ROPS with RIBS are shown below.

	Mode	Frequency [Hz]	
1	1.	0.	
2	2.	0.	
3	3.	4.317e-003	
4	4.	7.8062e-003	
5	5.	1.3685e-002	
6	6.	1.5841e-002	

	Mode	Frequency [Hz]	
1	1.	0.	
2	2.	0.	
3	3.	0.	
4	4.	4.5637e-003	
5	5.	6.4206e-003	
6	6.	7.3086e-003	

### 6. Results and Discussion

The analysis results of ROPS with RIBS and without RIBS are tabulated below.

Mode	Total Deformation at ROPS without RIBS	Total Deformation at ROPS with RIBS
1.	64.761 mm	45.169 mm
2.	34.206 mm	38.573 mm
3.	40.013 mm	45.79 mm
4.	43.773 mm	28.591 mm
5.	61.433 mm	28.232 mm
6.	66.98 mm	37.135 mm

# 7. Conclusion

1. The impact tests are made on the ROPS and the non-linear structural deformation results are formulated. But few plastic deformations may occur which can be neglected.

2. When the ROPS is subjected to the calculated loads, the nonlinear structural deformation is observed.

3. The ROPS with gusset, having cross section and dimension with least effect of the loading conditions were considered for the design and analysis aspects. The behavior of the ROPS is observed by FEA analysis at the ANSYS software.

4. The analysis of the ROPS concludes that the conditions during rolling over of the heavy machines doesn't collapse the structure.

5. The results proves that non-linear structural deformations are within the desirable limits and the ROPS with gusset satisfies the ISO 3471 standards.

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