

Miniaturized Band Pass Filter in Substrate Integrated Waveguide Technology

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Abstract

Miniaturization is an important criteria in the selection of devices for next generation communication systems. A novel miniaturization technique for an inductive post filter is investigated in this paper. Miniaturization is not so popular in inductive post Substrate Integrated Waveguide (SIW) filter and so considerable amount of research is to be done in this domain. A band pass filter in SIW technology using inductive posts is realized and further analyses are carried out. The insertion loss in the pass band is found to be 0.5 dB and the return loss is 22 dB. In this paper, we investigate the use of slow wave technology for miniaturization. Unlike the conventional SIW, the slow wave SIW topology requires a double layer substrate with internal metallized vias introduced in the bottom layer connected to the bottom conductive plane. The number of rows of internal metallized vias was chosen based on a parametric study. The proposed miniaturization technique shows that the SIW filter is 21.6 % and 34.6 % miniaturized in size and area respectively. The response of the filter covers Ka band and hence is suitable for satellite communication application. A quality factor of 506 is achieved for the miniaturized filter.

Keywords: *Slow wave; internal blind vias; band pass filter; SIW*

1. Introduction

Recent decades have witnessed evolution of various technologies for the development of microwave and millimeter wave components. With rapid development of such systems, performance requirements of passive band pass filters (as an essential part in these systems) are steadily increasing. SIW is a favorable choice to design band pass filters in microwave and millimeter wave frequencies. With its compact nature and low loss characteristics, SIW has attracted scientists and researchers working in the microwave and millimeter wave domains. SIW components inherit almost all advantages of conventional wave-guides such as complete shielding, low loss, high quality-factor and high power-handling capability overcoming their possible disadvantages such as large size and high fabrication cost. Similar to micro-strip and coplanar lines, SIW components are compact, light, easy to fabricate, flexible, and cost effective. SIW band pass filters could be designed using Complementary split ring resonators (CSRR). Here the high pass nature of SIW together with the band stop nature of CSRR is considered for the band pass response [1-4]. Band pass filter with SIW could also be realized using Defected Ground Structures (DGS). The basic concept is similar to obtaining band pass response using SIW and CSRR [5 -6]. Band pass filter with a combination of CSRR and DGS in SIW is also proposed [2]. Introducing inductive posts and irises in SIW can also result in a band pass filter [7-13,16,19]. The next generation telecommunication systems have a great demand for compact devices which made miniaturization an important criteria. A few techniques for miniaturization are illustrated in [1-6,16,23]. In [1,3], compact

size was achieved by incorporating the CSRR, resulting in an increased electrical length, thereby giving a band pass filter in the lower GHz range. In [2,4], miniaturization was made possible by the presence of DGS in the structure. Another approach for miniaturization in SIW components is by exploiting the concept of half mode as studied in [5,6,16] where a size reduction of at least 50 % is possible. In [1-6, 16], cavity filters were dealt with where the amount of losses will be less < 2 dB. Dealing with open ended structures at higher frequencies > 30 GHz is little challenging as more losses account into. In this paper, the authors propose a technique to achieve size reduction for SIW inductive post band pass filter (an open ended structure) by using a phenomenon of separation of electric and magnetic fields. In [23], capacitance and inductance are due to proximity coupling in terms of fringe fields whereas in the proposed work they are due to the physical separation between electric and magnetic fields. In this work, we design a SIW band pass filter using inductive posts and propose a new technique for filter miniaturization known as slow wave phenomenon. The concept of slow wave, not used before for miniaturization of inductive post band pass filter, shows that it is possible to achieve size reduction, while maintaining almost the same filter characteristics. The paper is organized as follows. Section 2 deals with basics of SIW structure followed by Section 3 illustrating basic SIW filter design. Section 4 describes slow-wave effect. It also contains performance comparison between basic SIW filter and slow wave SIW filter performances is shown. Full wave simulation based on a Finite Difference Time Domain (FDTD) package is used for analyzing the structure. Finally, the work is concluded in Section 5.

2. SIW Structure

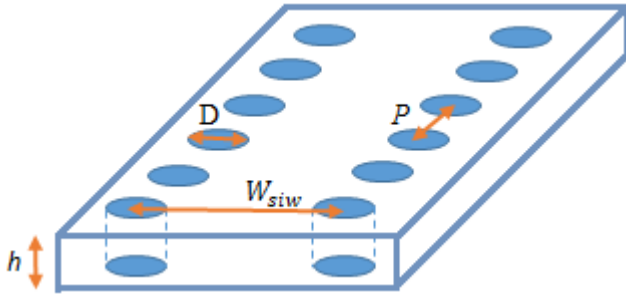


Figure 1: Basic SIW structure

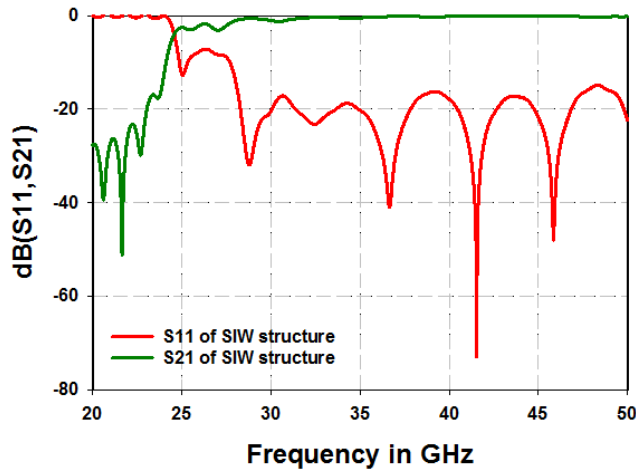


Figure 2: Frequency Response of SIW structure

Basic SIW structure consists of a substrate of height h , with top and bottom metallic conductive layers and lateral vias as shown in Figure 1. Lateral vias act as electric wall for the wave guide structure [15,18]. Like any wave guiding structure, it acts as a high pass filter with a lower cut-off frequency, as shown in Figure 2. The SIW considered in this work is designed for a cut off frequency of 25 GHz as apparent from its S21 component of frequency response. Rogers RO5880 substrate with a relative permittivity of 2.2 is used for the filter analysis. Other design parameters considered are, height of the substrate, $h = 0.254$ mm, diameter of via, $D = 0.25$ mm, distance between vias, pitch, $P = 0.4$ mm and width of SIW, $W_{siw} = 4$ mm.

3. Siw Band Pass Filter Design

The basic SIW filter discussed above is considered for designing a band pass filter. The filter layout is as shown in Figure 3. Tapered sections are used for proper impedance matching. The tapered sections also help in mode conversion between micro-strip feed and SIW. The mode present in the former is Transverse Magnetic (TM) and that present in latter is Transverse Electric (TE). Introducing inductive posts into the basic SIW filter converts the high pass into a band pass response. The equivalent circuit of the inductive post is as shown in Figure 4. The effect of introducing inductive posts in basic wave-guide could be referred in [8,9,12,22]. The inductive posts together with basic SIW wave-guide gives a band pass response [22]. The diameters of the inductive posts and distance between adjacent posts were optimized in order to achieve a perfect pass band. The frequency response of the basic SIW filter is as shown in Figure 5. The insertion loss in pass band is 0.5 dB, return loss is 22 dB and 3 dB bandwidth is 2.3 GHz.

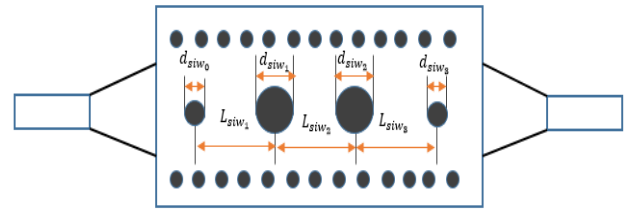


Figure 3: Basic SIW filter layout

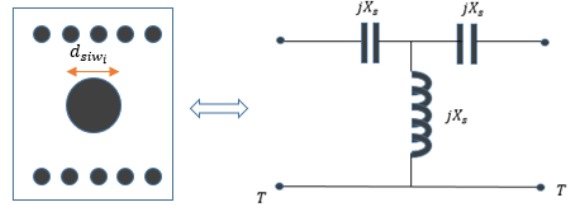


Figure 4: Equivalent circuit of an inductive post in SIW filter

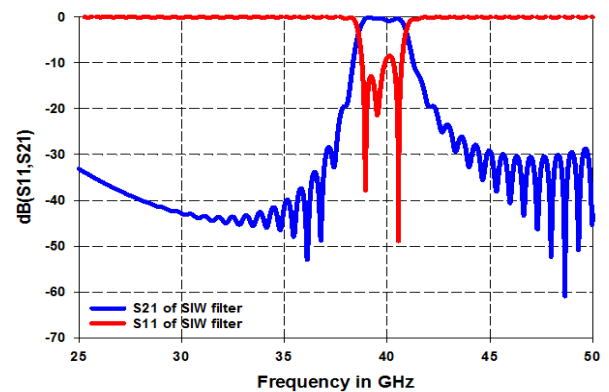


Figure 5: Frequency response of SIW filter

4. Slow Wave Siw Filter Design

Introducing blind vias in the pre-designed filter can reduce the filter size thus resulting in a slow wave SIW band pass filter. The slow wave concept is based on physical separation of electric and magnetic fields [15]. A lateral view of slowwave SIW filter is shown in Figure 6. The electric field is present in the top substrate of height h_1 and the magnetic field is present all around the internal blind vias. The internal vias in the substrate 2 act as reactive loading. Substrate 1 is an isolating layer preventing short circuiting between the circuits to be hosted by the slow wave structure [20]. Circuits and slow wave structure together are essentially planar in nature and can be fabricated by the standard Printed Circuit Board (PCB) technology.

The number of rows of internal vias to be used was based on a parametric study. Analysis was done using five rows and three rows of internal vias. The value of S21 with five rows of internal vias was below 10 dB whereas it was around 2.5 dB with three rows of internal blind vias. This means that the amount of losses is more with five rows of internal vias in comparison with three rows of internal blind vias. So, further analysis was carried out using three rows of internal blind vias. Introducing blind internal vias beneath the feeds was done by investigating the effect on a simple

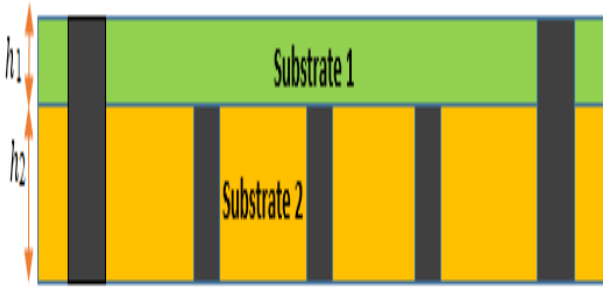


Figure 6: Lateral view of slow wave SIW structure

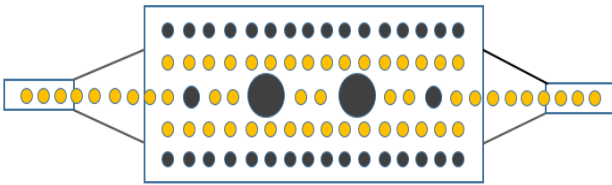


Figure 7: Slow wave SIW filter structure

micro-strip line since input is fed to the filter using a micro-strip line. Analysis showed that the internal vias need to be given just beneath the feed thereby reducing fabrication complexity and cost. Hence single row of internal vias is used in the feed sections. The final slow wave SIW band pass filter layout is shown in Figure 7.

The slow wave phenomenon leads to an increase in the effective inductance and capacitance associated with the structure as shown in Figure 8. The increase in inductance and capacitance also makes the structure para-electric and paramagnetic in nature by increasing the effective permittivity ϵ and effective permeability μ [20]. This is illustrated in Equations (1-4). Thus, the internal blind vias introduced inside the filter separate the electro-magnetic field, thereby slowing the wave, while increasing the permittivity and also permeability, as a result reducing the longitudinal and lateral dimensions. In fact the center frequency of SIW filter decreased from 39.5 GHz to 33.5 GHz, thereby shifting the center frequency by 6 GHz.

$$L' = L'_0 + \Delta L \tag{1}$$

$$C' = C'_0 + \Delta C \tag{2}$$

$$\mu_{eff} = \frac{L'}{\mu_0} \tag{3}$$

$$\epsilon_{eff} = \frac{C'}{\epsilon_0} \tag{4}$$

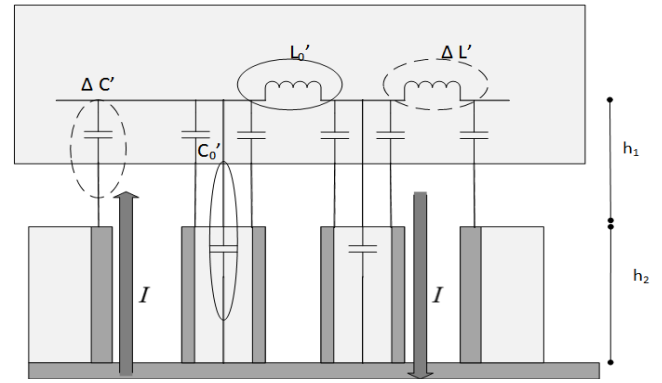
where, L'_0 represents the inductance of the basic filter without slow wave.

L' represents the lumped inductance of the filter after incorporating slow wave.

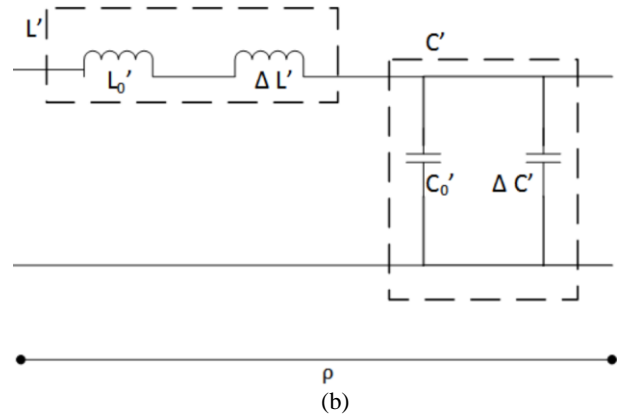
C'_0 represents the capacitance of the basic filter without slow wave.

C' represents the capacitance of the filter with slow wave.

This shows that a filter of smaller size, which was originally designed for higher frequency band (here 39.5 GHz) is now being used in a slightly lower frequency (here 33.5 GHz) with the same small size. This is apparent from Figure 9 which shows a comparison of the filter performance with and without the slow wave. It could be observed from the comparison that the insertion loss is



(a)



(b)

Figure 8: (a) Lumped circuit with effective circuit elements. (b) Complete lumped element equivalence for a unit cell

lower by 2 dB and bandwidth is wider by 0.5 GHz. Quality factor and group delay are important parameters in filters. Quality factor of the SW SIW band pass filter is 506. A comparison of group delay of filters is shown in the Figure 10. The value of group delay in the slow wave filter is less compared to the value in the filter without slow wave. This shows that the wave is longer time to travel from one port to the other port in the slow wave filter. The delay is added due to the physical separation of the electric and magnetic fields in the structure. Thus the slow wave concept is also validated from the values of group delay in both filters.

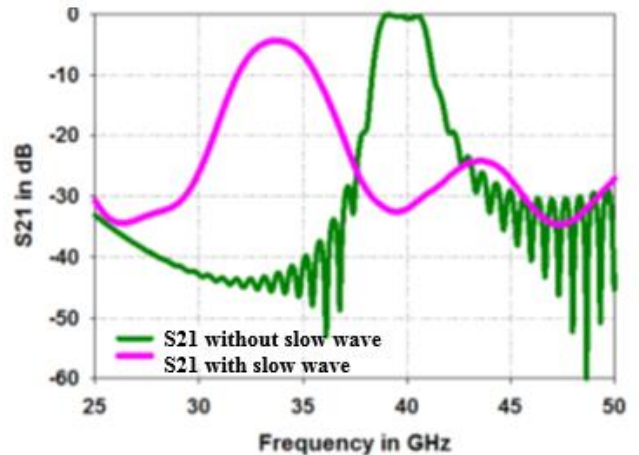


Figure 9: Comparison of transmission characteristics

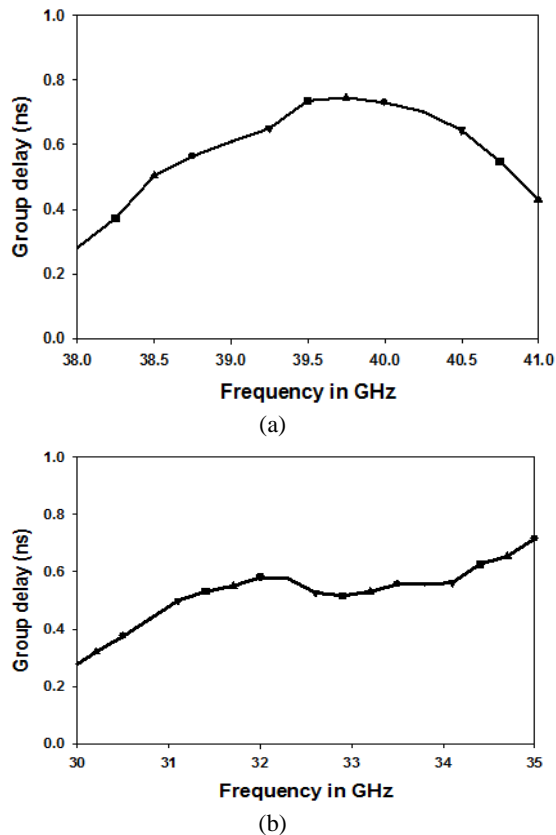


Figure 10: (a) Group delay in SIW band-pass filter (b) Group delay in SW SIW band-pass filter.

5. Conclusion

A miniaturized band pass inductive post filter in SIW technology is presented in this paper. The miniaturization was achieved using slow wave phenomenon. The slow wave technique was investigated with a double layer topology, wherein several rows of internal metallized vias are introduced in the bottom layer connected to the bottom conducting plane. The number of rows of internal metallized vias was chosen with a parametric study. The concept of slow wave, not used before for miniaturization of inductive post band pass filter, shows that it is possible to achieve smaller longitudinal dimensions resulting in an area reduction, by almost maintaining the same filter characteristics. Analysis showed that the SIW filter is 21.6% and 34.6% miniaturized in size and area respectively. The response of the filter spans the Ka band, hence, the filter can be used for satellite communication application. A quality factor of 506 is achieved for the miniaturized filter.

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