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Research paper



Flexural Behavior of Rolled Steel I Beam with Different Stiffener Position

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Abstract

Economy, ease and speed of construction are the main factors for using steel as a building material. In this paper conventional hot rolled steel I-beam sections are considered as the main flexural member of industrial buildings. The main goal is to increase the load carrying capacity of the beam with inverted w shape stiffener condition at centre. The initiative was to identify the maximum load behaviour and deflection of steel beams with stiffener in the web. The performance of such beams has been considered only for vertical loads. Hot rolled steel beam of ISMB 100 with stiffener were tested to failure experimentally. The beams were simply supported at the ends and subjected to a 2 equal concentrated load applied at one third of span from both ends. The deflection at centre of beam and various failure patterns are studied. All the beams were analyzed by the finite element method by using general finite element analysis software ANSYS and the results were compared with those obtained experimentally. The finite element results for deformation and ultimate strength shows good agreement with the corresponding values observed in the experiments. At last, a comparative study was carried out using finite element method to examine that which type of beam gives best performance during loading. The numerical results indicate that the use of hot rolled I section with stiffener is an economical and advantageous choice.

Keywords: Horizontal and vertical stiffener, Rolled steel section, Inclined stiffener, Flexural strength, etc..

1. Introduction

Laterally stable steel beams can fail only by (a) flexure (b) shear (c) bearing, assuming the local buckling of slender components does not occur. These three conditions are the criteria for limit state design of steel beams. Steel beams would also become unserviceable due to excessive deflection and it is classified as a limit state of serviceability.the factored design moment m at any section, in a beam due to external actions shall satisfy

> $M \le md$ Where md = design bending strength of the section

Members subjected to predominant bending shall have adequate design strength to resist concentrated force, shear force and bending moment imposed upon and their combinations Further, the members shall satisfy the deflection limitation presented as serviceability criteria. Member subjected to other forces in addition to bending or biaxial bending shall be designed. The effective span of a beam shall be taken as the distance between the centre to centre of supports, except where the point of application of the reaction is taken as eccentric at the support. It shall be permissible

to take the effective span as the length between the assumed lines of the reactions.Lateral-torsional buckling is a limit-state of structural usefulness where the deformation of a beam changes from predominantly in-plane deflection to a combination of lateral deflection and twisting while the load capacity remains first constant, before dropping off due to large deflections. The analytical aspects of determining the lateral-torsional buckling strength are quite complex, and close form solutions exist only for the simplest cases.

2. Objective

(i)The effect of intermediate and inclined lateral stiffeners on load carrying capacity of simply supported hot rolled steel I-beam under various load combinations.

(ii) Load carrying capacity of beam, maximum deflection, stressstrain behavior, curvature behavior, maximum stresses in beam and stiffener have to be analyzed.

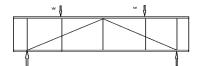
(iii) A series of beams modeled using 3d-finite element software like ansys is used to analyze the behavior of beam.

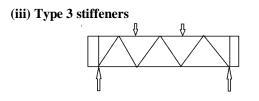
(iv) A theoretical design results, analytic results along with experimental results have been compared and final results are arrived.

3. Stiffener Outline

(I) Type 1 Stiffener

(Ii) Type 2 Stiffeners





4. Theoretical Report

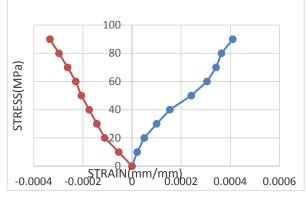
| Designation | Values | | | |
|-----------------------------------|----------------------|--|--|--|
| code | Is800:2007 | | | |
| Section type | Girder beam | | | |
| Loading type | Udl | | | |
| Span | 20m | | | |
| Dead load | 20KN/m | | | |
| Live load | 250KN/m | | | |
| Self weight | 18KN/m | | | |
| Ultimate load | 432KN/m | | | |
| Maximum BM | 21.6E9Nmm | | | |
| Maximum SF | 4320KN | | | |
| Overall depth | 2500mm | | | |
| Depth of web | 2400mm | | | |
| Thickness of web | 12mm | | | |
| Thickness of flange | 50mm | | | |
| Breadth of flange | 500mm | | | |
| Outstand of flange | 244mm | | | |
| B/t _f | 4.88 | | | |
| Classification | Plastic | | | |
| Plastic section modulus | 78.53E6 cu.mm | | | |
| Designation | Values | | | |
| Elastic section modulus | 70.4E6 cu.mm | | | |
| Moment of inertia(elastic) | 88E9 mm ⁴ | | | |
| Plastic moment capacity | 27.85E9 nmm | | | |
| d/t _w | 206 | | | |
| Spacing of stiffener | 3000mm | | | |
| C/d | 1.25 | | | |
| K _v | 11.6 | | | |
| Poisson ration | 0.3 | | | |
| Young modulus | 2E5 MPa | | | |
| Elastic critical shear stress | 52.42MPa | | | |
| Non dimensional slenderness ratio | 1.65 | | | |
| Shear stress(nominal) | 53.01MPa | | | |
| Critical force | 1526KN | | | |
| Margin of unsafety | 2794KN | | | |
| Designation | Values | | | |
| Limited moment of resistance | 4.09E9 Nmm | | | |
| Moment in tension field | 991.6E6 Nmm | | | |
| Force in tension field | 4.156E6 N | | | |
| Additional force due to moment in | 330KN | | | |
| tension field | | | | |
| Total design force | 4650KN | | | |
| Longitudinal shear | 2100KN | | | |
| Design load on EBS(end bearing | 4650KN | | | |
| stiffener) | | | | |
| Breadth of stiffener | 200mm | | | |
| Thickness of stiffener | 25mm | | | |
| Area of stiffener | 10000 sq mm | | | |
| Web crippling | 340KN | | | |
| T 1 1' 4 '1 4' | | | | |
| Load distribution | 1V:2.5H | | | |
| Total bearing strength | 1V:2.5H 4960KN | | | |
| | | | | |

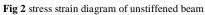
| MOI of axis level | 291.42E6 mm4 | | |
|--------------------------------------|-----------------------------------|--|--|
| Radius of gyration | 112.85mm | | |
| Slenderness ratio | 14.8 | | |
| Designation | Values | | |
| Buckling class | С | | |
| Direct compression | 225.5 MPa | | |
| Compression load | 5159 KN | | |
| Design load on its | 3024KN | | |
| Minimum MOI | 3.98E6 mm4 | | |
| Stiffener force due to external load | 2540KN | | |
| Direct compression | 224.5MPa | | |
| Compression load | 3538KN | | |
| Minimum MOI | 20.76E6 mm4 | | |
| Stiffener requirements | Satisfied limit conditions as per | | |
| | code | | |
| Connection (EBS and web) | Provide 40mm weld @150mm c/c | | |
| Connection (HS and web) | Provide 40mm weld @300mm c/c | | |
| Deflection | 78.23mm | | |

5. Experimental Report (1:20)

(I) Steel Beam without Stiffener







(Ii) Stiffener Beam 1



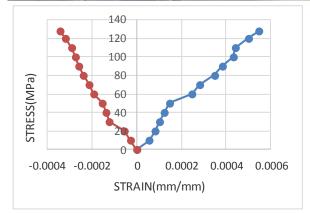


Fig 3 stress strain diagram for stiffened beam 1 $\,$

(Iii) Stiffened Beam 2



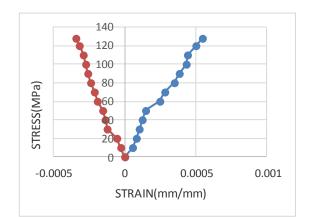


Fig 4 stress strain diagram for stiffened beam 2

(Iv)Stiffener Beam 3



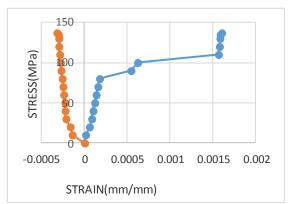
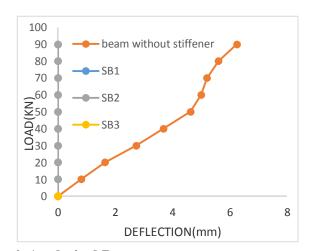


Fig 5 stress strain diagram for stiffened beam 3

(V) Deflection Comparison



6. Analytical Report

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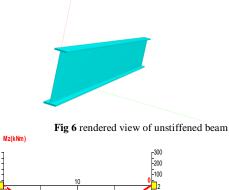
200

100

1<mark>_</mark> 100

200 -300 -

(i) Unstiffened Beam (Using STADDPRO)



15

-265

E100 E200 E300

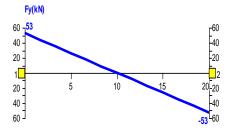


Fig 6: BM and SF diagram of unstiffened beam

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| 1 Beam * Node | Displacement | Beam | All L/C 1 SELF WE | Relative Disp Dist m G 0.000 5.000 10.000 15.000 20.000 D 0.000 | blacement / x mm 0.000 -0.000 -0.000 -0.000 0.000 0.000 | Max Relat y mm 0.000 -0.716 -1.006 -0.716 0.000 0.000 | ive Displac z mm 0.000 0.000 0.000 0.000 0.000 0.000 | ements / Resultan mm 0.000 0.71 1.000 0.71 0.000 0.000 67.58 |
| Beam & Node | Displacement | Beam | All L/C 1 SELF WE | Relative Disp Dist m G 0.000 10.000 15.000 20.000 D 0.000 5.000 | Diacement / mm 0.000 -0.000 -0.000 0.000 0.000 0.000 -0.000 | Max Relat y mm 0.000 -0.716 -1.006 -0.716 0.000 0.000 -67.582 | ive Displac mm 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | ements / Resultan mm 0.00 0.71 1.00 0.71 0.00 |

(Ii) Stiffened Beams (ANSYS)

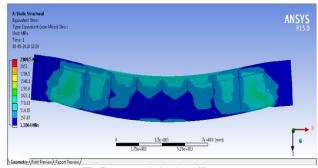


Fig 7 stress variation in stiffened beam

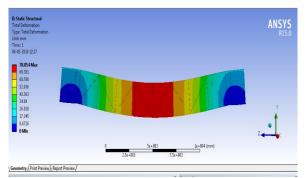


Fig 8 deflection in stiffened beam

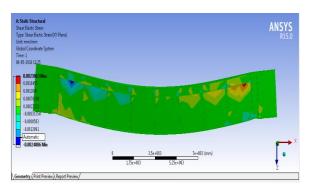


Fig 9 strain variation in stiffened beam

7. Result and Discussion

(i) Load carrying capacity of beam

- (a) Without stiffener =90 KN(b) Type 1 stiffener =102KN
- (c) Type 2 stiffener =128KN
- (d) Type 3 stiffener =137KN

(ii) Comparative results

| AD | AS | ED | ES |
|-------|---------------------------------|---|---|
| (mm) | | (mm) | |
| | | | |
| 94.88 | 0.00186 | 125 | 0.00041 |
| | | | |
| 91.66 | 0.00191 | 85.66 | 0.00085 |
| | | | |
| 85.26 | 0.00193 | 81.23 | 0.0012 |
| | | | |
| 78.66 | 0.00203 | 76.25 | 0.0019 |
| | (mm) 94.88 91.66 85.26 | (mm) 94.88 0.00186 91.66 0.00191 85.26 0.00193 | (mm) (mm) 94.88 0.00186 125 91.66 0.00191 85.66 85.26 0.00193 81.23 |

Note:

Ad=analytic deflection As=analytic strain Ed=experimental deflection(1:20) Es=experimental strain(1:20) (iii) Estimation of material cost(as per field application)

(a) Beam with no stiffener

Volume of beam =1.576 cubic metre Unit weight of steel =7850kg/cub m Weight of beam = 12371.6 kg Cost of steel per kg =rs.60 Total cost = 7.42 lakhs

(b) Beam with type 1 stiffener

Volume of beam =1.824 cubic metre Unit weight of steel =7850 kg/cub m Weight of beam =14318.4 kg Cost of steel per kg =rs.60 Total cost =8.6 lakh

(c) Beam with type 2 stiffener

Volume of beam =1.856 cubic metre Unit weight of steel =7850 kg/cub m Weight of beam =14569.6 kg Cost of steel per kg =rs.60 Total cost =8.74 lakh

(d) Beam with type 3 stiffener

Volume of beam =1.923cubic metre Unit weight of steel =7850kg/ cub m Weight of beam =15095.5 kg Cost of steel per kg =rs.60 Total cost =9.5 lakh

8. Conclusion

(i) The load carrying behaviour of type 3 stiffener beam is 20% higher than type 1 stiffener, 10% higher than type 2 stiffener and 41% higher than beam with no stiffener.

(ii) The deflection behaviour of type 3 stiffener beam is5% higher than type 2 stiffener and 10% higher than type 1 stiffener and 15% higher than beam with no stiffener.

(iii) For higher strength purpose, type 3 stiffener beam is preferable but for both economical and strength purpose, type 2 stiffener beam is preferable.

(iv) The above results should be completely compared and concluded theoretically, analytically and experimentally (1:20).

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