

Dry Sliding Wear Behavior of B₄C and Graphite Particulates Reinforced A356 Alloy Composites

Pankaj R Jadhav¹, B R Sridhar², Madeva Nagara³, Jayasheel I Harti⁴, V Auradi⁵

¹*Assistant Professor, Department Of Mechanical Engineering, East Point College Of Engineering And Technology, Bangalore-560049, Karnataka, India

²Professor, Department Of Mechanical Engineering, South East Asian Engineering College, Bangalore-560049, Karnataka, India

³Design Engineer, Aircraft Research And Design Centre, HAL, Bangalore-560037, Karnataka, India

⁴Assistant Professor, Department Of Mechanical Engineering, East Point College Of Engineering And Technology, Bangalore-560049, Karnataka, India

⁵Associate Professor, Department Of Mechanical Engineering, Siddaganga Institute Of Technology, Tumkur-587102, Karnataka, India

*Corresponding Author E-Mail: Pankaj4phd@gmail.com

Abstract

The present work manages readiness of the composites by mix stirring method. A356 amalgam 4 wt. % of B₄C and A356-4 wt. % of Graphite and A356-4% B₄C-4% Graphite hybrid composites were readied. To enhance the wetting and uniform conveyance of the particles, fortifications were preheated to a temperature of 500 Degree Celsius. The arranged MMCs are subjected to examining SEM instrument which affirms the homogenous uniform appropriation of smaller scale B₄C and Graphite particles in the lattice combination without agglomeration. The wear protection of arranged composites was examined by performing dry sliding wear test utilizing DUCOM made stick on plate mechanical assembly. The tests were directed at a consistent heap of 3kg and sliding separation of 4000m over a speed of 100, 200 and 300 rpm. So also the other arrangement of investigations were led at consistent sped of 300 rpm and sliding separation of 4000m and with changing heap of 1kg, 2kg, and 3kg. The outcomes demonstrated that the wear protections of the composites were improved than the lattice material.

Keywords: A356 Alloy; B₄C; Graphite; Microstructure; Wear

1. Introduction

Hybrid composites are those materials which have in excess of one fortifying material in lattice; this expansion of in excess of one strengthening material is completed to bestow the properties which other material does not have. Essential purpose behind creating composites with enhanced properties contrasted with customary material is a result of the request in light weight materials in present day period [1, 2]. The particulate strengthened grid demonstrate isotropic properties not at all like fiber fortified composites, likewise creation of particulate fortified metal framework composite is straightforward than get control driving strands over metal network utilizing regular throwing strategy. Subsequently, particulate fortified metal framework composites are broadly being utilized as a part of a few segments like Aerospace, Automotive, Marine, Sports and different utilities [3, 4].

The use of the MMC's in a few applications is be-reason for the enhanced mechanical and tribological properties when contrasted and ordinary compounds. The examinations have uncovered the impact of support on wear protection of composites; pottery like Silicon carbide (SiC), Aluminum oxide (Al₂O₃), Boron carbide (B₄C), Titanium carbide (TiC) utilized as strengthening material which oppose the measure of plastic distortion in metal lattice composites [5, 6].

The wear rate at first is low which winds up extreme in later stages as hard particulates increment the temperature around 40°C - 50°C, as the wear rate relies upon temperature parameter too. The

investigations demonstrate that as the volume division of particulates in framework stage increment the wear protection tend to increment and additionally the particles which are not reinforced legitimately with lattice eliminate pull effortlessly their by expanding the wear rate of MMC.

A Baradeswaran et al. [7] has demonstrated that the wear rate of aluminum combination is endless supply of upto 5 wt. % of graphite and further expansion builds the wear rate of composite. In the investigation it is likewise demonstrated that the tribological conduct is expanded as Graphite itself goes about as self greasing up material in dry sliding conditions. Blaza Stojanovic et al. [8] has chipped away at tribological conduct of A356 compound fortified with 10 wt. % Silicon carbide and 3 wt. % of Graphite cross breed MMC, the hybrid composite confer unrivaled attributes in dry sliding conditions and wear rate of crossover composite is constantly not as much as base metal lattice. Ritesh Raj et al. [9] has demonstrated that circulation of particulates in Aluminum compound is even and uniform with small bunching at higher wt% of B₄C particulates. Adalet Zeren [10] has demonstrated that expansion of Graphite to Al-SiC composite declines the hardness and thickness of composite however enhances wear and oil properties of the composite.

In the present work wear conduct of A356 amalgam strengthened with 4 wt. % of Boron Carbide and 4 wt. % of Graphite and furthermore hybrid metal grid composites were examined by leading wear test utilizing pin on disc contraption.

2. Experimental Details

Table 1 Chemical composition of A356 Alloy

Element	Element
Magnesium	0.29
Silicon	7.20
Iron	0.18
Copper	0.02
Zinc	0.01
Manganese	0.01
Titanium	0.11
Nickel	0.01
Aluminium	Bal

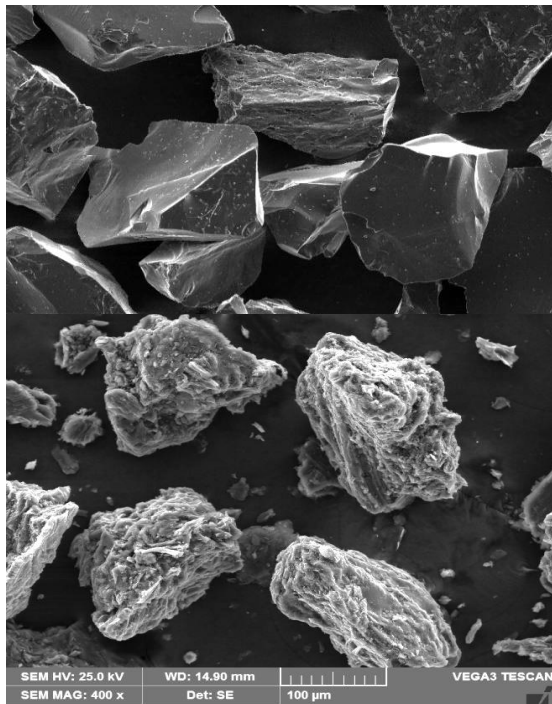


Fig.1a: Showing the scanning electron microphotographs of B₄C

Fig. 1b: Showing the SEM microphotographs of graphite particles

In the present investigation, A356 composite with the normal density of 2700 kg/m³ was utilized as a framework material. The con-coction composition of the network material is given in Table1. B₄C with normal density of 2520 kg/m³ and graphite particles with 2200 kg/m³ were utilized as fortifications. Figure 1 a-b demonstrate the B₄C and graphite particles of size 80-100 microns utilized as a part of the investigation.

At first B₄C and graphite particulates were preheated for 500°C. In the present work, an endeavor has been made to contemplate the wear properties of as cast A356 compound, A356-4% B₄C, A356-4% Graphite and A356-4% B₄C-4% Graphite crossover composites. In-itially required measure of charge or framework material was set in a graphite pot, which was put in electric protection heater at a temperature of around 730 degree Celsius. After entire dissolving of A356 amalgam framework, degassing was done by utilizing Solid Hexa Chloroethane [10], which expels undesirable adsorbed gases from the soften. Once degassing is finished, the pre-warmed B₄C support particles were brought into lattice novelty which includes two-arrange increments of rein-forcement amid liquefy mixing [11]. A nonstop blending process was done amid expansion of support into network. Ordinarily for all composite planning, blending speed was principle retained at 300rpm. Following 5 minutes of consistent blending, whole liquid metal was filled solid metal bite the dust. Essentially, A356-Graphite composites and A356-B₄C-Graphite hybrid composites were set up by

same course. The readied composites were mama chined and tried for small scale auxiliary investigations. The composites revealed uniform scattering of B₄C and graphite particles in the structure, wear direct of as cast A356 combination and its composites were surveyed by ASTM G99 standard.

The dry sliding wear conduct of as cast A356 compound and A356-B₄C-Graphite composites were assessed utilizing a pin on-circle wear mechanical assembly at room temperature as per ASTM G99 standard. Pins of length 30 mm and distance across 8mm were set up from the cast tests. The trials were led at a consistent sliding velocity of 300rpm and sliding separation of 4000m over a differing heap of 1Kg, 2Kg, and 3Kg. Also tries were led at a consistent heap of 3Kg and sliding separation of 4000m over a changing sliding pace of 100, 200 and 300rpm. The cleaned surface of the stick was slide on a solidified chromium steel circle. A computerizes data collection helped information securing framework was utilized to screen the loss of tallness. Wear esteem is introduced as far as stature misfortune.

3. Results and Discussion

3.1 Microstructural Studies

Fig. 2 a-d indicates microstructure of as cast A356, A356-4 wt. % B₄C, A356-4 wt. % graphite and A356-4% B₄C-4% Graphite hybrid composites. By and large the lattice frameworks in aluminum base combination cast particulate incorporate, Al-Si, Al-Cu or Al-Zn-Mg composites which have eutectic write stage out-lines. The hypoeutectic, eutectic and hypereutectic Al-Si base composites are habitually utilized as networks for particulate fortifications including graphite, alumina and silicon carbide. The conceivable interfaces in these Al-Si network composite frameworks can be between the essential α -aluminum and support, or between essential silicon and fortification, or between the eutectic of aluminum-silicon and the support. Figure2 b-d uncovered that there is genuinely uniform dissemination of B₄C and graphite particulates all through the grid combination. It is likewise watched that porosity is lower. Further, from the SEM micrographs, it can be seen that there is great holding between the network and the get control forcement particulates coming about over better load exchange from the framework to support material [12].

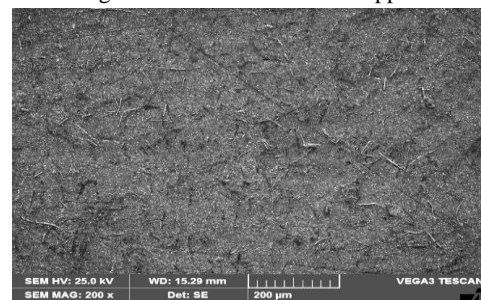


Fig 2: (a)

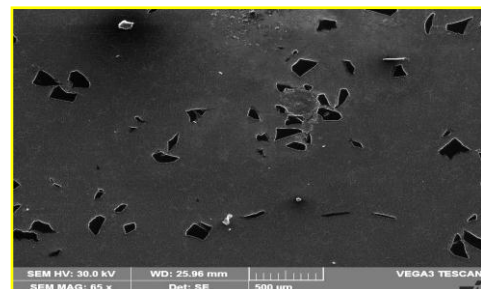


Fig 2: (b)

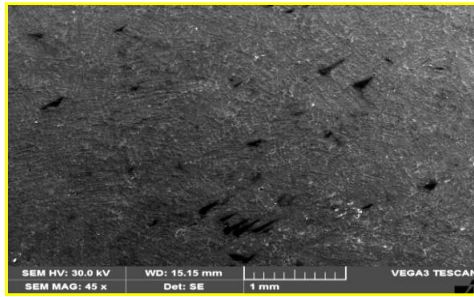


Fig 2: (c)

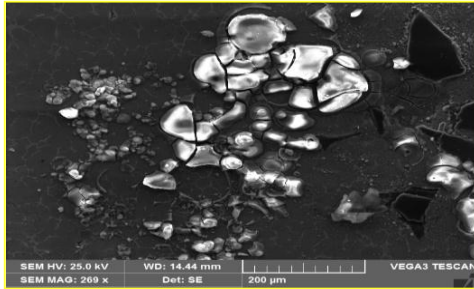


Fig 2: (d)

Fig 2: Showing scanning electron microphotographs of (a) as cast A356 alloy (b) A356-4 wt. % of B₄C (c) A356-4 wt. % of Graphite (d) A356-4 wt. % of B₄C-Graphite hybrid composites

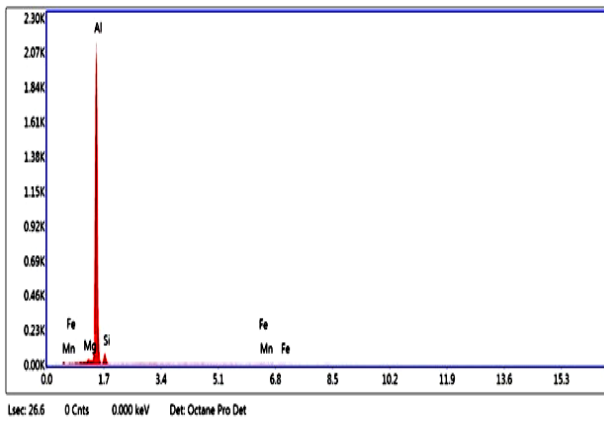


Fig 3: (a)

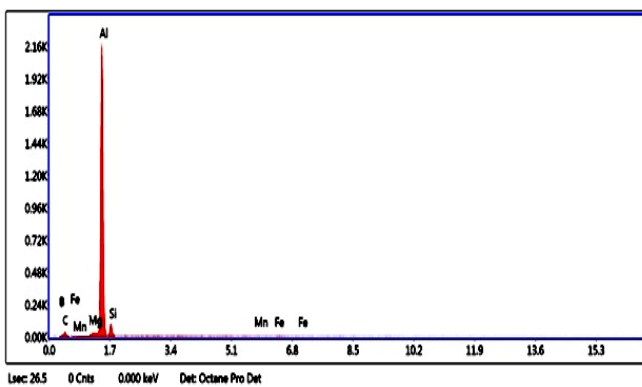


Fig 3: (b)

Fig. 3: Showing energy dispersive spectrographs of (a) as cast A356 alloy (b) A356-4 wt. % of B₄C-Graphite hybrid composites

Figure 3 a-b are energy dispersive X-Ray spectrographs of as cast A356 amalgam and A356-4wt. % of B₄C and graphite composites separately. The EDS examination affirmed the nearness of B₄C and Graphite in the Al lattice composite. The nearness of B₄C and graphite appears as Boron (B) and Carbon (C), which is clear from the EDS diagram 3b.

3.2. Wear Behavior

The variation of wear loss at steady 300rpm sliding speed and changing loads of 1Kg, 2Kg and 3Kg is as appeared in fig. 4. Applied load influences the wear of A356 compound and the composites fundamentally and is the most overwhelming component controlling the wear conduct. The wear misfortune changes with the typical load and is altogether lower if there should arise an occurrence of composites. With increase in loads there is higher wear incident for lattice compound and the composites. However at all the heaps considering wear protection of the composites is superior to the structure blend. At higher burdens and the progress to separate wear the surface temperature surpasses a basic esteem. So as connected load increments eventually there is an expansion in the wear misfortune for both the fortified and unreinforced composite materials. The variety of wear loss of the lattice amalgam and its composites with 4 wt. % of B₄C-Graphite content is appeared in fig. 4 underneath.

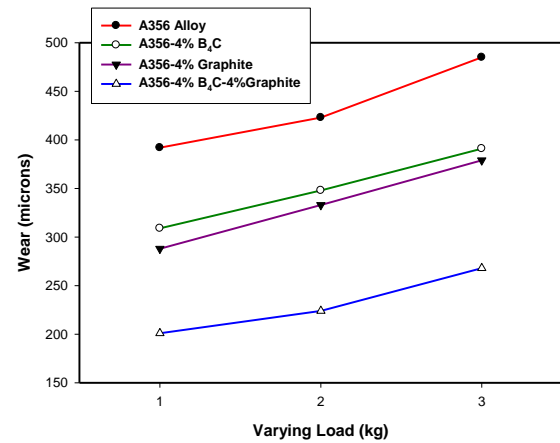


Fig. 4: Showing wear of A356 alloy and its composites at constant 300rpm speed and varying loads

Fig. 5 demonstrates the variety of wear loss of AA356 grid combination and its B₄C-Graphite composites at consistent 3Kg load and differing sliding paces. With an expanding speed i.e. 100, 200, and 300 rpm, there is an expansion in the wear misfortune for both framework compound and its composites. However at all the sliding paces examined, the wear loss of the composite was much lower when contrasted and the grid combination. Additionally expanded wear rate with expanded sliding rate is because of warm softening of the composite. Then again the expanded temperature at higher sliding paces can cause extreme plastic misshapening of the mating surfaces prompting structure high strain rate sub-surface disfigurement [13, 14]. The expanded rate of sub-surface disfigurement builds the contact region by crack, and fracture of ill tempers. Subsequently this prompts improved delamination adding to upgrade the wear rate.

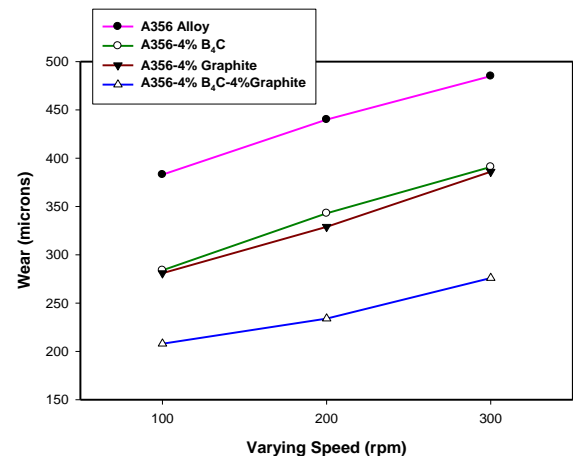


Fig. 5: Showing wear of A356 alloy and its composites at constant 3kg load and varying speeds

The change in the wear protection of the composites with B₄C support can be credited to the change in the hardness of the composites and enhanced hardness brings about the decline in the wear loss of the composites [15]. Further, Graphite strengthened A356 compound composites were displayed high wear protection contrasted with A356 combination and B₄C composites. This in-wrinkle in wear protection is basically because of self grease conduct of graphite, which goes about as a strong lubricant. The wear conduct of cross breed composites was still more contrasted with all composites, because of joined impact of B₄C and graphite particulates.

4. Conclusions

The present work on handling and assessment of wear of A356-B₄C-Graphite metal lattice composite by dissolve blending has prompted following conclusions. A356 combination based composites have been effectively created by dissolve blending technique joined with preheating of particles. The SEM microphotographs of composites uncovered genuinely uniform conveyance of fortification particulates in the A356 metal grid and EDS spectrographs affirmed the nearness of B₄C and Graphite particles. The expansion of B₄C and Graphite particles to Al compound framework enhances the wear protection of the composite. The wear misfortune is commanded by stack factor and sliding rate. The expansion of burdens and sliding velocities prompts a huge increment in the wear misfortune. The A356-4% B₄C-4% Graphite cross breed composites have indicated bring down wear misfortune when contrasted with that saw in as cast A356 combination, 4 wt. % B₄C and 4 wt. % Graphite fortified composites grid.

References

- [1] Dinesh Patidar, R. S. Rana, Effect of B₄C particle reinforcement on the various properties of aluminium matrix composites, *Materials Today*, 4, 2981–2988, 2017.
- [2] Pankaj R Jadhav, B R Sridhar, Madeva Nagaral, Jayasheel Harti, Evaluation of mechanical properties of B₄C and graphite particulates reinforced A356 alloy hybrid composites, *Materials Today Proceedings*, 4, 9, pp. 9972-9976, 2017.
- [3] G.G.Sozhamannan, M.Muttharasan, K.Kaviarasan, S.Balasivanandha Prabhu, V. S. K. Venkatachopathy, Influence of silicon on performance of al/sic composites, *Applied Mechanics and Materials*, Vols. 592-594, pp 421-425, 2014.
- [4] J.M. Carrapichano, J.R. Gomes, R.F. Silva, Tribological behaviour of Si₃N₄-BN ceramic materials for dry sliding applications, *Wear*, 253, 1070–1076, 2002.
- [5] Bekir Sadik Unlu, Investigation of tribological and mechanical properties Al₂O₃-SiC reinforced Al composites manufactured by casting or P/M method, *Materials and Design*, 29, 2002–2008, 2008.
- [6] R.N. Rao, S. Das, Wear coefficient and reliability of sliding wear test procedure for high strength aluminium alloy and composite, *Materials and Design*, 31, 3227–3233, 2010.
- [7] A. Baradeswaran, A. Elaya Perumal, Effect of Graphite on Tribological and Mechanical Properties of AA7075 Composites, *Tribology Transactions*, 58, 1040-2004, 2015.
- [8] Blaza Stojanovic, Miroslav Babic, Nenad Miloradovic, Slobodan Mitrovic, Tribological behaviour of a356/10sic/3gr hybrid composite in dry-sliding conditions, *Materials and technology*, 49, 1580-2949, 2015.
- [9] Ritesh Raj, Dineshsingh G. Thakur, Qualitative and quantitative assessment of microstructure in Al-B₄C metal matrix composite processed by modified stir casting technique, *Archives of Civil and Mechanical Engineering*, 16, 1644-9665, 2016.
- [10] Adalet Zeren, Effect of the graphite content on the tribological properties of hybrid Al/SiC/Gr composites processed by powder metallurgy, *Industrial Lubrication and Tribology*, 0036-8792, pp. 262 – 268, 2014
- [11] Jayasheel I Harti, T B Prasad, Madeva Nagaral, Pankaj Jadhav and V Auradi, Microstructure and dry sliding wear behavior of Al2219-TiC composites, *Materials Today Proceedings*, 4, 10, pp. 11004-11009, 2017.
- [12] K.Rajkumar, P.Rajan, Effect of Boron Carbide and Graphite on Machining Characteristics of Aluminium Boron Carbide Composite, *Applied Mechanics and Materials*, Vol. 592-594, 181-185, 2014.
- [13] G. Sabatini, L. Ceschini, C. Martini, J.A. Williams, I.M. Hutchings, Improving sliding and abrasive wear behaviour of cast A356 and wrought AA7075 aluminium alloys by plasma electrolytic oxidation, *Materials and Design*, 31, 816–828, 2010.
- [14] Madeva Nagaral, B K Shivananda, Jayachandran, V Auradi and S A Kori, Effect of SiC and Graphite particulates addition on wear behavior of Al2219 alloy hybrid composites, *IOP Conf. Series: Materials Science and Engineering*, 149, 012108, 2016.
- [15] V. C. Uvaraja, N. Natarajan, Optimization of Friction and Wear Behaviour in Hybrid Metal Matrix Composites Using Taguchi Technique, *Journal of Minerals and Materials Characterization and Engineering*, 11, pp. 757-768, 2012.